Appendix 5.13-1 Noise and Vibration Technical Memo

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Building Construction w/Pile Driving Noise Levels (LEQ)

	Distance to Nearest	Combined Predicted		Reference Emission Noise Levels (L _{max}) at 50	Usage
Location	Receptor in feet	Noise Level (L _{eg} dBA)	Equipment	feet ¹	Factor ¹
threshold	947	65.0	Compactor (ground)	80	0.4
Center	0	#NUM!	Generator	82	0.4
Staging Area	0	#NUM!	Crane	85	0.16
			Dump Truck	84	0.4
			Compressor (air)	80	0.4
			Front End Loader	80	0.4
			Backhoe	80	0.4
			Man Lift	85	0.4
			Impact Pile Driver	95	0.2

Ground Type	hard
Source Height	8
Receiver Height	5
Ground Factor ²	0.00

Predicted Noise Level ³	L _{eq} dBA at 50 feet ³
Compactor (ground)	76.0
Generator	78.0
Crane	77.0
Dump Truck	80.0
Compressor (air)	76.0
Front End Loader	76.0
Backhoe	76.0
Man Lift	81.0
Impact Pile Driver	88.0

Combined Predicted Noise Level (L_{eq} dBA at 50 feet)

90.5

Sources:

 $^{\rm 1}$ Obtained from the FHWA Roadway Construction Noise Model, January 2006. Table 1.

² Based on Figure 6-5 from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 6-23).

³ Based on the following from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 12-3).

 $L_{eq}(equip) = E.L.+10*log (U.F.) - 20*log (D/50) - 10*G*log (D/50)$

Where: E.L. = Emission Level;

U.F.= Usage Factor;

G = Constant that accounts for topography and ground effects (FTA 2006: pg 6-23); and



Building Construction (No Pile Driving) Construction Noise Levels (LEQ)

Distance to Nea	Distance to Nearest	Combined Predicted		Reference Emission Noise Levels (L _{max}) at 50	Usage
Location	Receptor in feet	Noise Level (L _{eg} dBA)	Equipment	feet ¹	Factor ¹
threshold	324	70.0	Compactor (ground)	80	0.4
Center	0	#NUM!	Generator	82	0.4
Staging Area	0	#NUM!	Crane	85	0.16
			Dump Truck	84	0.4
			Front End Loader	80	0.4
			Man Lift	85	0.4

Ground Type	hard
Source Height	8
Receiver Height	5
Ground Factor ²	0.00

Predicted Noise Level ³	L _{eq} dBA at 50 feet ³
Compactor (ground)	76.0
Generator	78.0
Crane	77.0
Dump Truck	80.0
Front End Loader	76.0
Man Lift	81.0

Combined Predicted Noise Level (L_{eq} dBA at 50 feet)

86.2

Sources:

 $^{\rm 1}$ Obtained from the FHWA Roadway Construction Noise Model, January 2006. Table 1.

² Based on Figure 6-5 from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 6-23).

³ Based on the following from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 12-3).

 $L_{eq}(equip) = E.L.+10*log (U.F.) - 20*log (D/50) - 10*G*log (D/50)$

Where: E.L. = Emission Level;

U.F.= Usage Factor;

G = Constant that accounts for topography and ground effects (FTA 2006: pg 6-23); and



Roadway Construction Noise Levels (LEQ)

	Distance to Nearest	Combined Predicted		Reference Emission Noise Levels (L _{max}) at 50	Usage
Location	Receptor in feet	Noise Level (L _{eg} dBA)	Equipment	feet ¹	Factor ¹
threshold	641	65.0	Paver	85	0.4
Center	0	#NUM!	Roller	85	0.4
Staging Area	0	#NUM!	Concrete Mixer Truck	85	0.4
			Front End Loader	80	0.4
			Flat Bed Truck	84	0.4

Ground Type	hard
Source Height	8
Receiver Height	5
Ground Factor ²	0.00

Predicted Noise Level ³	L _{eq} dBA at 50 feet ³
Paver	81.0
Roller	81.0
Concrete Mixer Truck	81.0
Front End Loader	76.0
Flat Bed Truck	80.0

Combined Predicted Noise Level (L_{eq} dBA at 50 feet)

87.2

Sources:

 $^{\rm 1}$ Obtained from the FHWA Roadway Construction Noise Model, January 2006. Table 1.

² Based on Figure 6-5 from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 6-23).

³ Based on the following from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 12-3).

 $L_{eq}(equip) = E.L.+10*\log (U.F.) - 20*\log (D/50) - 10*G*\log (D/50)$

Where: E.L. = Emission Level;

U.F.= Usage Factor;

G = Constant that accounts for topography and ground effects (FTA 2006: pg 6-23); and

ASCENT

Utility Construction Noise Levels (LEQ)

	Distance to Nearest Combined Predicted			Reference Emission Noise Levels (L _{max}) at 50	Usage
Location	Receptor in feet	Noise Level (L _{eq} dBA)	Equipment	feet ¹	Factor ¹
threshold	715	65.0	Man Lift	85	0.4
Center	0	#NUM!	Crane	85	0.4
Staging Area	0	#NUM!	Flat Bed Truck	84	0.4
			Front End Loader	80	0.4
			Auger Drill Rig	85	0.4
			Excavator	85	0.4

Ground Type	hard
Source Height	8
Receiver Height	5
Ground Factor ²	0.00

Predicted Noise Level ³	L _{eq} dBA at 50 feet ³
Man Lift	81.0
Crane	81.0
Flat Bed Truck	80.0
Front End Loader	76.0
Auger Drill Rig	81.0
Excavator	81.0

Combined Predicted Noise Level (L_{eq} dBA at 50 feet)

88.1

Sources:

 $^{\rm 1}$ Obtained from the FHWA Roadway Construction Noise Model, January 2006. Table 1.

² Based on Figure 6-5 from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 6-23).

³ Based on the following from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 12-3).

 $L_{eq}(equip) = E.L.+10*log (U.F.) - 20*log (D/50) - 10*G*log (D/50)$

Where: E.L. = Emission Level;

U.F.= Usage Factor;

G = Constant that accounts for topography and ground effects (FTA 2006: pg 6-23); and

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Site Prep Construction Noise Levels (LEQ)

	Distance to Nearest	Combined Predicted		Reference Emission Noise Levels (L _{max}) at 50	Usage
Location	Receptor in feet	Noise Level (L _{eq} dBA)	Equipment	feet ¹	Factor ¹
threshold	665	65.0	Dozer	85	0.4
Center	0	#NUM!	Grader	85	0.4
Staging Area	0	#NUM!	Dump Truck	84	0.4
			Excavator	85	0.4
			Backhoe	80	0.4
			Front End Loader	80	0.4

Ground Type	hard
Source Height	8
Receiver Height	5
Ground Factor ²	0.00

Predicted Noise Level ³	L _{eq} dBA at 50 feet ³
Dozer	81.0
Grader	81.0
Dump Truck	80.0
Excavator	81.0
Backhoe	76.0
Front End Loader	76.0

Combined Predicted Noise Level (L_{eq} dBA at 50 feet)

87.5

Sources:

 $^{\rm 1}$ Obtained from the FHWA Roadway Construction Noise Model, January 2006. Table 1.

² Based on Figure 6-5 from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 6-23).

³ Based on the following from the Federal Transit Noise and Vibration Impact Assessment, 2006 (pg 12-3).

 $L_{eq}(equip) = E.L.+10*\log (U.F.) - 20*\log (D/50) - 10*G*\log (D/50)$

Where: E.L. = Emission Level;

U.F.= Usage Factor;

G = Constant that accounts for topography and ground effects (FTA 2006: pg 6-23); and

Equipment Description	Acoustical Usage Factor (%)	Spec 721.560 Lmax @ 50ft (dBA slow)	Actual Measured Lmax @ 50ft (dBA slow)	No. of Actual Data Samples (count)	Spec 721.560 LmaxCalc	Spec 721.560 Leq	Distance	Actual Measured LmaxCalc	Actual Measured Leq
Auger Drill Rig	20	85	84	36	79.0	72.0	100	78.0	71.0
Backhoe	40	80	78	372	74.0	70.0	100	72.0	68.0
Bar Bender	20	80	na	0	74.0	67.0	100		
Blasting	na	94	na	0	88.0	74.0	100	77.0	74.0
Boring Jack Power Unit Chain Saw	50 20	80 85	83 84	1 46	74.0 79.0	71.0 72.0	100 100	77.0 78.0	74.0 71.0
Clam Shovel (dropping)	20	93	87	40	79.0 87.0	80.0	100	81.0	71.0
Compactor (ground)	20	80	83	57	74.0	67.0	100	77.0	74.0
Compressor (air)	40	80	78	18	74.0	70.0	100	72.0	68.0
Concrete Batch Plant	15	83	na	0	77.0	68.7	100		
Concrete Mixer Truck	40	85	79	40	79.0	75.0	100	73.0	69.0
Concrete Pump Truck	20	82	81	30	76.0	69.0	100	75.0	68.0
Concrete Saw	20	90	90	55	84.0	77.0	100	84.0	77.0
Crane	16	85	81	405	79.0	71.0	100	75.0	67.0
Dozer Drill Big Truck	40 20	85 84	82 79	55 22	79.0 78.0	75.0 71.0	100 100	76.0 73.0	72.0 66.0
Drill Rig Truck Drum Mixer	20 50	80	80	1	78.0	71.0	100	73.0	71.0
Dump Truck	40	84	76	31	74.0	74.0	100	74.0	66.0
Excavator	40	85	81	170	79.0	75.0	100	75.0	71.0
Flat Bed Truck	40	84	74	4	78.0	74.0	100	68.0	64.0
Front End Loader	40	80	79	96	74.0	70.0	100	73.0	69.0
Generator	50	82	81	19	76.0	73.0	100	75.0	72.0
Generator (<25KVA, VMS s	50	70	73	74	64.0	61.0	100	67.0	64.0
Gradall	40	85	83	70	79.0	75.0	100	77.0	73.0
Grader	40	85	na	0	79.0	75.0	100	01.0	77.0
Grapple (on Backhoe) Horizontal Boring Hydr. Jac	40 25	85 80	87 82	1 6	79.0 74.0	75.0 68.0	100 100	81.0 76.0	77.0 70.0
Hydra Break Ram	10	90	na	0	84.0	74.0	100	70.0	70.0
Impact Pile Driver	20	95	101	11	89.0	82.0	100	95.0	88.0
Jackhammer	20	85	89	133	79.0	72.0	100	83.0	76.0
Man Lift	20	85	75	23	79.0	72.0	100	69.0	62.0
Mounted Impact Hammer	20	90	90	212	84.0	77.0	100	84.0	77.0
Pavement Scarafier	20	85	90	2	79.0	72.0	100	84.0	77.0
Paver	50	85	77	9	79.0	76.0	100	71.0	68.0
Pickup Truck	40	55	75	1	49.0	45.0	100	69.0	65.0
Pneumatic Tools	50 50	85 77	85 81	90 17	79.0 71.0	76.0 68.0	100 100	79.0 75.0	76.0 72.0
Pumps Refrigerator Unit	100	82	73	3	71.0	76.0	100	67.0	67.0
Rivit Buster/chipping gun	20	85	79	19	79.0	70.0	100	73.0	66.0
Rock Drill	20	85	81	3	79.0	72.0	100	75.0	68.0
Roller	20	85	80	16	79.0	72.0	100	74.0	67.0
Sand Blasting (Single Nozzle	20	85	96	9	79.0	72.0	100	90.0	83.0
Scraper	40	85	84	12	79.0	75.0	100	78.0	74.0
Shears (on backhoe)	40	85	96	5	79.0	75.0	100	90.0	86.0
Slurry Plant	100	78	78	1	72.0	72.0	100	72.0	72.0
Slurry Trenching Machine	50	82	80	75	76.0	73.0	100	74.0	71.0
Soil Mix Drill Rig Tractor	50 40	80 84	na na	0 0	74.0 78.0	71.0 74.0	100 100		
Vacuum Excavator (Vac-tru		85	85	149	78.0	74.0	100	79.0	75.0
Vacuum Street Sweeper	10	80	82	19	74.0	64.0	100	76.0	66.0
Ventilation Fan	100	85	79	13	79.0	79.0	100	73.0	73.0
Vibrating Hopper	50	85	87	1	79.0	76.0	100	81.0	78.0
Vibratory Concrete Mixer	20	80	80	1	74.0	67.0	100	74.0	67.0
Vibratory Pile Driver	20	95	101	44	89.0	82.0	100	95.0	88.0
Warning Horn	5	85	83	12	79.0	66.0	100	77.0	64.0
Welder / Torch	40	73	74	5	67.0	63.0	100	68.0	64.0

Source:

FHWA Roadway Construction Noise Model, January 2006. Table 9.1

U.S. Department of Transportation

CA/T Construction Spec. 721.560



KEY: Orange cells are for input.

Grey cells are intermediate calculations performed by the model. Green cells are data to present in a written analysis (output).

STEP 1: Determine units in which to perform calculation.

- If vibration decibels (VdB), then use Table A and proceed to Steps 2A and 3A.
- If peak particle velocity (PPV), then use Table B and proceed to Steps 2B and 3B.

STEP 2A: Identify the vibration source and enter the reference vibration level (VdB) and distance.

STEP 3A: Select the distance to the receiver.

Table A. Propagation of vibration	decibels (VdB) with distance
-----------------------------------	------------------------------

Noise Source/ID	Reference Noise Level									
	vibration level	distance								
	(VdB)	@	(ft)							
Impact pile driver	104	@	25							
vibratory roller	95	@	25							

STEP 2B: Identify the vibration source and enter the reference peak particle velocity (PPV) and distance.

Attenuated Noise Level at Receptor										
vibration level		distance								
(VdB)	@	(ft)								
65.0	@	500								
79.8	@	80								

STEP 3B: Select the distance to the receiver.

Attenuated Noi	Attenuated Noise Level at Receptor											
vibration level		distance										
(PPV)	@	(ft)										
0.197	@	55										
0.210	@	25										

Table B. Propagation of peak particle velocity (PPV) with distance Naise Source (ID)

Noise Source/ID	Referenc	e No	oise Level
	vibration level		distance
	(PPV)	@	(ft)
Impact pile driver vibratory roller	0.644 0.210	@ @	25 25

Notes:

Computation of propagated vibration levels is based on the equations presented on pg. 12-11 of FTA 2006. Estimates of attenuated vibration levels do not account for reductions from intervening underground barriers or other underground structures of any type, or changes in soil type.

Sources:

Federal Transit Association (FTA). 2006 (May). Transit Noise and Vibration Impact Assessment. FTA-VA-90-1003-06. Washington, D.C. Available: http://www.fta.dot.gov/documents/FTA_Noise_and_Vibration_Manual.pdf>. Accessed: September 24, 2010.



Attenuation Calculations for Stationary Noise Sources

KEY: Orange cells are for input.

Grey cells are intermediate calculations performed by the model.

Green cells are data to present in a written analysis (output).

STEP 1: Identify the noise source and enter the reference noise level (dBA and distance).

STEP 2: Select the ground type (hard or soft), and enter the source and receiver heights.

STEP 3: Select the distance to the receiver.

Noise Source/ID	Reference	e Noi	ise Level	4	Attenuation C	haracteristics	Attenuated Noise Level at Receptor					
	noise level		distance	Ground Type	Source	Receiver	Ground		noise leve	I	distance	
	(dBA)	@	(ft)	(soft/hard)	Height (ft)	Height (ft)	Factor		(dBA)	@	(ft)	
Loading Dock Activity Leq (day)	77.0	@	100	soft	6	5	0.65		64.7	@	290	
Loading Dock Activity Leq (night)	77.0	@	100	soft	6	5	0.65		59.9	@	440	
HVAC leq (day)	70.0	@	50	soft	6	5	0.65		64.6	@	80	
HVAC Leq (night)	70.0	@	50	soft	6	5	0.65		59.9	@	120	

Notes:

Estimates of attenuated noise levels do not account for reductions from intervening barriers, including walls, trees, vegetation, or structures of any type.

Computation of the attenuated noise level is based on the equation presented on pg. 12-3 and 12-4 of FTA 2006.

Computation of the ground factor is based on the equation presentd in Figure 6-23 on pg. 6-23 of FTA 2006, where the distance of the reference noise leve can be adjusted and the usage factor is not applied (i.e., the usage factor is equal to 1).

Sources:

Federal Transit Association (FTA). 2006 (May). Transit Noise and Vibration Impact Assessment. FTA-VA-90-1003-06. Washington, D.C. Available: http://www.fta.dot.gov/documents/FTA_Noise_and_Vibration_Manual.pdf>. Accessed: September 24, 2010.

Existing Co	olse Spreadsheet Calculator															
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	ADT															
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	Wilson Aug from Concline State Archibeld Aug	4 740	40	00	112	00.00/	0.42%	0.00/	04.00/	E 40/	0.70/	575	7	15	21	
2	Wilson Ave from Carnelian St to Archibald Ave	4,740 5,190	40	88 88	112	98.8% 98.9%	0.42%	0.8%	84.8% 83.7%	5.4% 6.1%	9.7% 10.1%	57.5 59.5	9	15 20	31 43	68 92
	Wilson Ave from Archibald Ave to Haven Ave		45	94		_				-	10.1%		-		58	
3	Wilson Ave from Haven Ave to Milliken Ave Wilson Ave from Milliken Ave to Etiwanda Ave	7,860	45	94 88	106 112	98.4% 98.9%	0.67%	1.0% 0.7%	82.6%	7.0%	10.4%	61.5 55.7	12 5	27 11	24	125 51
4	Wilson Ave from Killiken Ave to City Limits	8,240	35	88	112	98.9%	0.43%	1.9%	82.8% 79.7%	6.2% 8.6%	11.0%	55.7	9	20	43	92
6	· · · · · · · · · · · · · · · · · · ·	3,470	35	94	112	_		0.5%			10.0%	59.5	3	20	43 15	32
7	Banyan St from Carnelian St to Archibald Ave Banyan St from Archibald Ave to Haven Ave	3,470	30	94	106	99.1% 99.3%	0.39%	0.5%	82.5% 77.6%	7.5%	10.0%	52.5	4	8	15	32
		9,690	45	94	106	_	0.32%	0.4%		10.5%	11.9%	62.9	16	34	72	156
8	Banyan St from Haven Ave to Milliken Ave Banyan St from Milliken Ave to Etiwanda Ave	10.530	45	94	106	99.3% 98.8%	0.31%	0.4%	73.4% 83.1%	6.7%	14.3%	62.5	15	34	69	156
10	Banyan St from Etiwanda Ave to Wardman Bollock Rd	8,210	45	94	106	98.8%	0.44%	0.8%	83.1% 79.7%	8.6%	10.2%	62.0	13	29	63	148
10					106	_							21	45		207
11	19th St from Carnelian St to Archibald Ave	17,050	45 45	88 88		98.8%	0.50%	0.7%	83.4%	6.0%	10.7%	64.8		45	96 92	197
	19th St from Archibald Ave to Haven Ave	15,630	45		112	98.7%	0.54%	0.8%	82.2%	7.4%	10.4%	64.5	20	42		
13 14	Base Line Rd from Carnelian St to Archibald Ave	22,550	40	88 88	112 112	98.1% 98.2%	0.67%	1.2%	82.4%	7.3%	10.2% 10.1%	64.8 64.5	21 20	44	96 91	206 197
14	Base Line Rd from Archibald Ave to Haven Ave Base Line Rd from Haven Ave to Milliken Ave	21,140 25,150	40	88	112	98.2%	0.69%	1.2%	81.5%	8.5% 7.5%	9.6%	66.7	20	59	128	275
15			50	82	118	_			82.9%				33	71	128	329
16	Base Line Rd from Milliken Ave to Etiwanda Ave Church St west of Archibald Ave	22,780 5,370	40	94	118	98.2% 98.5%	0.67%	1.1% 0.8%	81.0% 83.3%	8.4%	10.6% 9.7%	67.9 58.1	7	16	35	75
17	Church St from Archibald Ave to Haven Ave	9,060	40	88	108	_	0.72%			3.7%	11.0%	60.5	11	23	50	107
18		16,730	40	88	112	98.7% 97.9%	0.96%	0.7%	85.3% 79.4%	9.6%	11.0%	63.7	11	38	82	107
20	Church St from Haven Ave to Milliken Ave Church St from Milliken Ave to Day Creek Blvd	19,240	40	88	112	97.9%	1.00%	0.8%	79.4% 82.1%	9.6%	10.2%	65.4	23	38 49	106	228
20	· · · · · · · · · · · · · · · · · · ·	19,240	45	88	112	98.2%	0.96%	0.8%			9.2%	64.0	18	49 40	86	185
21	Church St from Day Creek Blvd to Etiwanda Ave Church St from Etiwanda Ave to East Ave	9,780	35	88	112	98.1%	0.96%	0.9%	83.0% 86.5%	7.8%	9.2%	58.9	8	18	39	84
22	Foothill Blvd from City Limits to Carnelian St/Vineyard Ave	32,820	45	88	112	97.6%	0.92%	1.5%	80.5% 77.9%	9.9%	10.3%	68.5	36	78	169	363
23	Foothill Blvd from Carnelian St/Vineyard Ave	31,300	45	82	112	97.8%	0.92%	1.5%	78.0%	9.9%	12.2%	68.4	36	78	165	356
24	Foothill Blvd from Archibald Ave to Haven Ave	32,420	50	88	118	97.7%	0.93%	1.4%	76.5%	9.7%	12.3%	69.8	45	96	207	446
26	Foothill Blvd from Haven Ave to Milliken Ave	32,420	50	82	112	97.4%	1.00%	1.4%	75.4%	11.2%	13.4%	70.9	53	113	207	526
20	Foothill Blvd from Milliken Ave to Day Creek Blvd	37,330	50	82	118	96.7%	1.14%	2.2%	73.6%	12.1%	14.3%	70.3	55	113	256	551
27	Foothill Blvd from Day Creek Blvd to Etiwanda Ave	45,190	50	82	118	95.8%	1.14%	3.0%	70.5%	13.8%	14.3%	72.6	68	113	316	681
28	Foothill Blvd from Etiwanda Ave to City Limits	34,430	50	88	118	95.8%	1.23%	2.5%	73.0%	12.7%	14.3%	72.8	52	113	243	524
30	Arrow Rte from City Limits to Vineyard Ave	19,710	45	88	112	96.5%	1.17%	2.3%	84.3%	5.6%	14.3%	66.1	25	54	117	253
30	Arrow Rte from Vineyard Ave to Archibald Ave	22,570	45	88	112	95.4%	1.05%	3.3%	79.7%	8.9%	11.4%	67.4	31	67	144	310
31	Arrow Rte from Archibald Ave to Haven Ave	22,570	45	88	112	95.4% 95.3%	1.26%	3.3%	79.7% 81.7%	7.6%	10.7%	67.9	31	72	144	310
32	Arrow Rte from Haven Ave to Milliken Ave	26,340	45 50	88	112	95.3%	2.12%	3.2%	81.7%	8.6%	10.7%	69.1	40	86	155	401
33	Arrow Rte from Haven Ave to Milliken Ave	24,300	50	88 94	112	94.4%	1.48%	3.5%	80.3% 78.0%	8.6%	11.1%	68.8	38	85	186	383
34	Arrow Rte from Etiwanda Ave to City Limits	20,140	50	94 88	106	96.4%	0.93%	1.3%	78.0% 81.4%	8.5%	10.1%	67.2	38	64	178	299
35	6th St from City Limits to Archibald Ave	10,940	45	94	112	97.7%	1.00%	2.6%	81.4% 82.4%	8.5% 7.4%	10.1%	63.6	30	37	81	174
30	6th St from Archibald Ave to Haven Ave	10,940	45	94	106	96.4% 96.0%	1.42%	2.6%	82.4% 81.7%	7.8%	10.2%	65.1	22	47	102	219
38	6th St from Haven Ave to Milliken Ave	14,860	45	88	108	96.7%	1.42%	2.0%	79.9%	9.0%	10.3%	65.1	22	47	102	219
38	6th St from Milliken Ave to Etiwanda Ave	13,870	35	88	112	95.5%	1.28%	2.1%	79.9% 88.1%	9.0%	7.9%	61.4	12	27	57	124
40	4th St from Archibald Ave to Haven Ave	13,870	50	88	112	95.5% 96.5%	1.83%	2.7%	80.0%	9.0%	11.0%	67.2	30	65	139	300
	4th St from Haven Ave to Haven Ave					-				-			30	84	139	300
41	4th St from Haven Ave to Milliken Ave	26,570	50	76	124	95.8%	1.41%	2.7%	85.1%	5.7%	9.2%	69.0	39	84	180	388

Traffic Noise Spreadsheet Calculator

ASCENT

Traffic N 2040 Cond	oise Spreadsheet Calculator litions															
Project:	Rancho Cucamonga GPU															
•	J. J					Input	t							Output		
	CNEL													•		
	Soft															
	ADT															
				Distan	nce to											
				Direct	ional											
	Segment Description and Location		Speed	Centerlin	e, (feet) ₄		Traffic Di	stribution	Characte	eristics		CNEL,	D	istance to C	Contour, (fe	et)₃
umber	Segment	ADT	(mph)	Near	Far	% Auto	% Medium	% Heavy	% Day	% Eve	% Night	(dBA) _{5,6,7}	75 dBA	70 dBA	65 dBA	60 dB
SEG ID																
1	Wilson Ave from Carnelian St to Archibald Ave	7,380	40	88	112	98.8%	0.42%	0.8%	84.8%	5.4%	9.7%	59.4	9	20	42	91
2	Wilson Ave from Archibald Ave to Haven Ave	8,490	45	88	112	98.9%	0.46%	0.6%	83.7%	6.1%	10.1%	61.6	13	27	59	127
3	Wilson Ave from Haven Ave to Milliken Ave	11,540	45	94	106	98.4%	0.67%	1.0%	82.6%	7.0%	10.4%	63.1	16	35	75	161
4	Wilson Ave from Milliken Ave to Etiwanda Ave	2,970	45	88	112	98.9%	0.43%	0.7%	82.8%	6.2%	11.0%	57.2	7	14	30	65
5	Wilson Ave from Etiwanda Ave to City Limits	12,480	35	88	112	97.4%	0.68%	1.9%	79.7%	8.6%	11.7%	61.3	12	26	56	121
6	Banyan St from Carnelian St to Archibald Ave	3,800	30	94	106	99.1%	0.39%	0.5%	82.5%	7.5%	10.0%	52.9	3	7	16	34
7	Banyan St from Archibald Ave to Haven Ave	3,970	30	94	106	99.3%	0.32%	0.4%	77.6%	10.5%	11.9%	53.4	4	8	17	36
8	Banyan St from Haven Ave to Milliken Ave	12,240	45	94	106	99.3%	0.31%	0.4%	73.4%	12.3%	14.3%	63.9	18	39	85	182
9	Banyan St from Milliken Ave to Etiwanda Ave	12,100	45	94	106	98.8%	0.44%	0.8%	83.1%	6.7%	10.2%	63.2	16	35	75	162
10	Banyan St from Etiwanda Ave to Wardman Bollock Rd	10,340	45	94	106	98.4%	0.61%	1.0%	79.7%	8.6%	11.8%	63.0	16	34	73	157
11	19th St from Carnelian St to Archibald Ave	20,840	45	88	112	98.8%	0.50%	0.7%	83.4%	6.0%	10.7%	65.6	24	51	110	236
12	19th St from Archibald Ave to Haven Ave	19,310	45	88	112	98.7%	0.54%	0.8%	82.2%	7.4%	10.4%	65.4	23	49	105	227
13	Base Line Rd from Carnelian St to Archibald Ave	26,170	40	88	112	98.1%	0.67%	1.2%	82.4%	7.3%	10.2%	65.4	23	49	106	228
14	Base Line Rd from Archibald Ave to Haven Ave	24,830	40	88	112	98.2%	0.67%	1.2%	81.5%	8.5%	10.1%	65.2	22	47	102	219
15	Base Line Rd from Haven Ave to Milliken Ave	32,780	45	82	118	98.2%	0.69%	1.1%	82.9%	7.5%	9.6%	67.8	33	71	152	328
16	Base Line Rd from Milliken Ave to Etiwanda Ave	34,870	50	82	118	98.2%	0.67%	1.1%	81.0%	8.4%	10.6%	69.7	44	94	203	437
17	Church St west of Archibald Ave	6,390	40	94	106	98.5%	0.72%	0.8%	83.3%	7.0%	9.7%	58.9	8	18	39	84
18	Church St from Archibald Ave to Haven Ave	13,540	40	88	112	98.7%	0.61%	0.7%	85.3%	3.7%	11.0%	62.2	14	30	65	140
19	Church St from Haven Ave to Milliken Ave	22,290	40	88	112	97.9%	0.96%	1.2%	79.4%	9.6%	11.0%	65.0	21	46	99	213
20	Church St from Milliken Ave to Day Creek Blvd	23,830	45	88	112	98.2%	1.00%	0.8%	82.1%	7.7%	10.2%	66.3	26	57	122	263
21	Church St from Day Creek Blvd to Etiwanda Ave	19,630	45	88	112	98.1%	0.96%	0.9%	83.0%	7.8%	9.2%	65.4	23	49	105	226
22	Church St from Etiwanda Ave to East Ave	12,360	35	88	112	98.8%	0.57%	0.6%	86.5%	3.2%	10.3%	60.0	10	21	46	99
23	Foothill Blvd from City Limits to Carnelian St/Vineyard Ave	38,620	45	88	112	97.6%	0.92%	1.5%	77.9%	9.9%	12.2%	69.2	40	87	188	405
24	Foothill Blvd from Carnelian St/Vineyard Ave to Archibald Ave	46,470	45	82	118	97.7%	0.93%	1.4%	78.0%	9.7%	12.3%	70.1	46	100	215	464
25	Foothill Blvd from Archibald Ave to Haven Ave	42,170	50	88	112	97.7%	0.92%	1.4%	76.5%	11.2%	12.4%	70.9	53	114	247	531
26	Foothill Blvd from Haven Ave to Milliken Ave	46,080	50	82	118	97.4%	1.00%	1.6%	75.4%	11.2%	13.4%	71.7	60	129	277	597
27	Foothill Blvd from Milliken Ave to Day Creek Blvd	50,790	50	82	118	96.7%	1.14%	2.2%	73.6%	12.1%	14.3%	72.6	68	146	314	676
28	Foothill Blvd from Day Creek Blvd to Etiwanda Ave	55,460	50	82	118	95.8%	1.23%	3.0%	70.5%	13.8%	15.7%	73.5	78	168	362	780
29	Foothill Blvd from Etiwanda Ave to City Limits	38,790	50	88	112	96.4%	1.17%	2.5%	73.0%	12.7%	14.3%	71.4	57	122	263	568
30	Arrow Rte from City Limits to Vineyard Ave	24,750	45	88	112	96.5%	1.05%	2.4%	84.3%	5.6%	10.1%	67.1	29	63	136	294
31	Arrow Rte from Vineyard Ave to Archibald Ave	26,320	45	88	112	95.4%	1.26%	3.3%	79.7%	8.9%	11.4%	68.1	34	74	160	344
32	Arrow Rte from Archibald Ave to Haven Ave	34,800	45	88	112	95.3%	1.43%	3.2%	81.7%	7.6%	10.7%	69.1	40	87	187	402
33	Arrow Rte from Haven Ave to Milliken Ave	30,900	50	88	112	94.4%	2.12%	3.5%	80.3%	8.6%	11.1%	70.1	47	101	219	471
34	Arrow Rte from Milliken Ave to Etiwanda Ave	34,960	50	94	106	96.4%	1.48%	2.1%	78.0%	10.3%	11.6%	70.2	48	103	222	479
35	Arrow Rte from Etiwanda Ave to City Limits	29,810	50	88	112	97.7%	0.93%	1.3%	81.4%	8.5%	10.1%	68.9	39	84	180	389
36	6th St from City Limits to Archibald Ave	13,370	45	94	106	96.4%	1.00%	2.6%	82.4%	7.4%	10.2%	64.5	20	43	92	199
37	6th St from Archibald Ave to Haven Ave	18,810	45	94	106	96.0%	1.42%	2.6%	81.7%	7.8%	10.5%	66.1	25	55	118	254
38	6th St from Haven Ave to Milliken Ave	21,570	45	88	112	96.7%	1.28%	2.1%	79.9%	9.0%	11.1%	66.7	28	60	129	278
39	6th St from Milliken Ave to Etiwanda Ave	18,220	35	88	112	95.5%	1.83%	2.7%	88.1%	4.1%	7.9%	62.6	15	32	69	148
40	4th St from Archibald Ave to Haven Ave	22,810	50	88	112	96.5%	1.29%	2.2%	80.0%	9.0%	11.0%	68.3	35	76	164	354
41	4th St from Haven Ave to Milliken Ave	36,230	50	76	124	95.8%	1.41%	2.7%	85.1%	5.7%	9.2%	70.4	48	103	221	477

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Citation # Citations

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- 3 Caltrans Technical Noise Supplement. 2009 (November). Equation (2-16), Pg 2-32.
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Federal Transit Administration Noise Impact Assessment Spreadsheet Copyright 2007 HMMH Inc. version: 7/3/2007

Noise Source Parameters

Receiver Parameters		
	Receiver:	Receiver 1
	Land Use Category:	2. Residential
	Existing Noise (Measured or Generic Value):	50 dBA

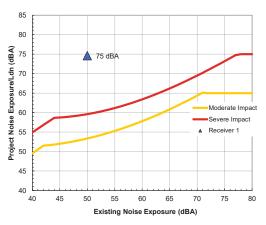
Number of Noise Sources: 2

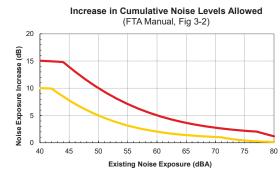
Project: Rancho Cucamong GPU

	Existing Ldn:	50 dBA
	Total Project Ldn:	75 dBA
	Total Noise Exposure:	75 dBA
	Increase:	25 dB
	Impact?:	Severe

Distance to Impact Contours	
Dist to Mod. Impact Contour	
(Sources 1+2):	860 ft
Dist to Sev. Impact Contour	
(Sources 1+2):	330 ft

Noise Impact Criteria (FTA Manual, Fig 3-1)





Moderate Impact Severe Impact Receiver 1

Noise Source Param	eters	Source 1
	Source Type:	Fixed Guideway
	Specific Source:	Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	1
	Speed (mph)	120
	Avg. Number of Events/hr	5.25
Nighttime hrs	Avg. Number of Locos/train	1
	Speed (mph)	120
	Avg. Number of Events/hr	3.75
Distance	Distance from Source to Receiver (ft)	33
	Number of Intervening Rows of Buildings	0
Adjustments		

Noise Source Parameters		Source 2	
	Source Type:	Fixed Guideway	
	Specific Source:	Transit warning device	
Daytime hrs			
	Speed (mph)	120	
	Avg. Number of Events/hr	5.25	
Nighttime hrs			
	Speed (mph)	120	
	Avg. Number of Events/hr	3.75	
Distance	Distance from Source to Receiver (ft)	33	
	Number of Intervening Rows of Buildings	0	
Adjustments			

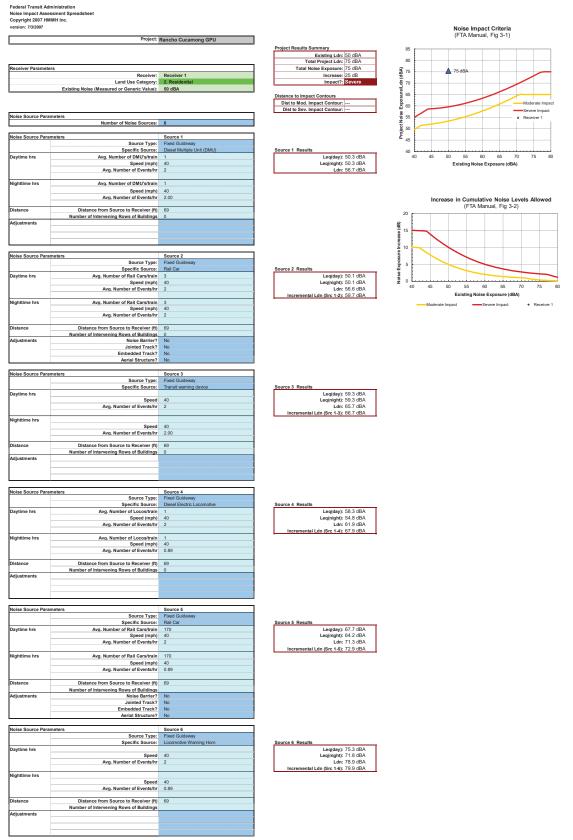
Source 2 Results	
	Leq(day): 63.5 dBA
	Leq(night): 62.0 dBA
	Ldn: 68.7 dBA

Incremental Ldn (Src 1-2): 74.6 dBA

Source 1 Results Leq(day): 68.1 dBA Leq(night): 66.6 dBA Ldn: 73.3 dBA

Federal Transit Administration Noise Impact As: Copyright 2007 version: 7/3/2007

	Proiect:	Rancho Cucamong GPU		(FTA Manual, Fig 3-1)
	10,000	rancho oucumony or o	Project Results Summary	85
			Existing Ldn: 50 dBA	
			Total Project Ldn: 75 dBA	80
Receiver Parameter			Total Noise Exposure: 75 dBA	₹ 75 ABA
	Receiver:	Receiver 1	Increase: 25 dB	
	Land Use Category: Existing Noise (Measured or Generic Value):		Impact?: Severe	fg 70
	Existing Noise (measured of Generic Value).	50 UBA	Distance to Impact Contours	Moderative Second
			Dist to Mod. Impact Contour:	Moderate
			Dist to Sev. Impact Contour:	🛱 60 - Severe li
Noise Source Parar				Severe li
	Number of Noise Sources:	3		
loise Source Parar		Source 1		410 50 C
volse Source Parar	Source Type:	Fixed Guideway		45
		Rail Transit Vehicle	Source 1 Results	40
Daytime hrs	Avg. Number of Transit Vehicles/train		Leq(day): 62.0 dBA	40 45 50 55 60 65 70 75
	Speed (mph)	40	Leq(night): 47.8 dBA	Existing Noise Exposure (dBA)
	Avg. Number of Events/hr	/5	Ldn: 60.9 dBA	
lighttime hrs	Avg. Number of Transit Vehicles/train	1	-	
J	Speed (mph)			
	Avg. Number of Events/hr			Increase in Cumulative Noise Levels All
				(FTA Manual, Fig 3-2)
Distance	Distance from Source to Receiver (ft) Number of Intervening Rows of Buildings	60		20
djustments	Noise Barrier?	No		
	Jointed Track?	No		Noise Exposure increase (db)
	Embedded Track?	No		ase
	Aerial Structure?	No		
Noise Source Parar	neters	Source 2		ŝ.
torse oource i arai	Source Type:	Fixed Guideway		so c
	Specific Source:	Rail Car	Source 2 Results	ш з
Daytime hrs	Avg. Number of Rail Cars/train	3	Leq(day): 66.8 dBA	oise
	Speed (mph) Avg. Number of Events/hr	40 75	Leq(night): 52.5 dBA Ldn: 65.6 dBA	40 45 50 55 60 65 70 7
	Avg. Number of Eventshi	15	Incremental Ldn (Src 1-2): 66.9 dBA	Existing Noise Exposure (dBA)
Nighttime hrs	Avg. Number of Rail Cars/train	3		
	Speed (mph)	40		
	Avg. Number of Events/hr	2.814814815		
Distance	Distance from Source to Receiver (ft)	60		
	Number of Intervening Rows of Buildings	0		
Adjustments	Noise Barrier?	No		
	Jointed Track? Embedded Track?	No No		
	Aerial Structure?	No		
	neters	Source 3		
loise Source Parar		Fixed Guideway	Course & Doculto	
loise Source Parar	Source Type:		Source 3 Results	
,		Transit warning device	Log(dout): 75.0 dBA	
,	Source Type: Specific Source:	Transit warning device 40	Leq(day): 75.9 dBA Leq(night): 61.7 dBA	
	Source Type:	40	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Paytime hrs	Source Type: Specific Source: Speed	40	Leq(night): 61.7 dBA	
Daytime hrs	Source Type: Specific Source: Speed Avg. Number of Events/hr	40 75	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed	40 75 40	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs	Source Type: Specific Source: Speed Avg. Number of Events/hr	40 75 40	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs Jighttime hrs	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed Avg. Number of Events/hr Distance from Source to Receiver (ft)	40 75 40 2.81 60	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs lighttime hrs Distance	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed Avg. Number of Events/hr	40 75 40 2.81 60	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs Nighttime hrs Distance	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed Avg. Number of Events/hr Distance from Source to Receiver (ft)	40 75 40 2.81 60	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Noise Source Paran Daytime hrs Nightlime hrs Distance Adjustments	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed Avg. Number of Events/hr Distance from Source to Receiver (ft)	40 75 40 2.81 60	Leq(night): 61.7 dBA Ldn: 74.8 dBA	
Daytime hrs Nighttime hrs Distance	Source Type: Specific Source: Speed Avg. Number of Events/hr Speed Avg. Number of Events/hr Distance from Source to Receiver (ft)	40 75 40 2.81 60	Leq(night): 61.7 dBA Ldn: 74.8 dBA	



Assumptions

Day

Brightine

			Peak HR		Off-Peak Hr	
			train/hr	PK HR/Day	train/hr	NON PK HR/Day
	Frequency	/	1	4	0.25	20
			Hr/period PK HR/Peric NN PK HR/Period			/Period
	Daytime	7am-10pm	15	2	13	5.25
	Night	10pm-7am	9	2	7	3.75
Gold Line	9					
			counted from sch.	every 12 min		
	<u>Night</u>	frequency	<u>10p-5:20a</u> 17	<u>5:20a-7am</u> 8.33	<u>Total</u> 25.33	<u>Tr/hr</u> 2.81
	Devi		Min/hr	Min/period	Freq. (min/hr)	Train/hr

60

Source Fehr & Peers 2021: email communication from Jason Pack to Dimitri Antoniou of Ascent on 4/26/2021

Gold Line Schedule (Oct, 2025)

Distance (ft) To Contour

12

75

	75 dBA Ldn	70 dBA Ldn	65 dBA Ldn	60 dBA Ldn	55 dBA Ldn
			fe	eet	
Brightline HSR	33	63	136	306	772
Gold Line Extension	60	129	281	632	1595
Metrolink	69	148	322	725	1828

900